



On the representation of capsizing in iceberg models



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ABSTRACT

Although iceberg models have been used for decades, they have received far more widespread attention in recent years, due in part to efforts to explicitly represent icebergs in climate models. This calls for increased scrutiny of all aspects of typical iceberg models. An important component of iceberg models is the representation of iceberg capsizing, or rolling. Rolling occurs spontaneously when the ratio of iceberg width to height falls below a critical threshold. Here we examine previously proposed representations of this threshold, and we find that there have been crucial flaws in the representation of rolling in many modeling studies to date. We correct these errors and identify an accurate model representation of iceberg rolling. Next, we assess how iceberg rolling influences simulation results in a hierarchy of models. Rolling is found to substantially prolong the lifespan of individual icebergs and allow them to drift farther offshore. However, rolling occurs only after large icebergs have lost most of their initial volume, and it thus has a relatively small impact on the large-scale freshwater distribution in comprehensive model simulations. The results suggest that accurate representations of iceberg rolling may be of particular importance for operational forecast models of iceberg drift, as well as for regional changes in high-resolution climate model simulations.

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1. Introduction

The drift and decay of icebergs has received increasing interest in recent years associated with several factors. (i) Icebergs pose a threat to high-latitude shipping, as well as to offshore hydrocarbon exploration efforts. The rapid retreat of Arctic sea ice and concurrent increases in oil and gas demands have increased shipping through the Arctic (Pizzolato et al., 2014) and discussions of drilling operations in the Arctic Ocean (Unger, 2014; Henderson and Loe, 2016). (ii) Global warming, and particularly high temperatures observed around Greenland and the Antarctic Peninsula, are being linked to increases in the flux of icebergs calving from glaciers and ice shelves. Calving rates are thus projected to accelerate during the coming decades (e.g., Rignot and Kanagaratnam, 2006; Copland et al., 2007; Rignot et al., 2011; Joughin et al., 2014). (iii) An increased incidence of icebergs is projected to impact regional ecosystems and oceanographic conditions (e.g., Vernet et al., 2012; Smith et al., 2013; Stern et al., 2015; Duprat et al., 2016). (iv) Icebergs carry and release freshwater far from the calving source (Silva et al., 2006; Rackow et al., 2017), and they can affect the large-scale ocean circulation (e.g., Martin and Adcroft, 2010;

Stern et al., 2016); (v) As an extreme example of this, the release of massive armadas of icebergs from the Laurentide Ice Sheets during the Heinrich Events of the last glacial period are believed to have affected Earth's climate globally (see e.g., Broecker, 1994; Stokes et al., 2015). In light of these factors, icebergs are being increasingly represented in climate models of varying complexity, ranging from Earth System Models of Intermediate Complexity (EMICs) (e.g., Jongma et al., 2009; 2013; Bügelmayr et al., 2015), to high-resolution ocean models (e.g., Marsh et al., 2015; Merino et al., 2016), to state-of-the-art comprehensive global climate models (GCMs) (e.g., Martin and Adcroft, 2010; Hunke and Comeau, 2011; Stern et al., 2016).

The fate of an iceberg is determined by a number of processes. Iceberg trajectories are strongly dependent on the shape and size of the iceberg, so as an iceberg decays, the forces acting on it change. Some of the decay is continuous and takes place in the form of gradual ablation. However, there are several iceberg processes that are inherently less continuous and complicate model representations of iceberg drift and decay, such as fracture and breakup, grounding events, and capsizing. This study focuses on the latter phenomenon.

Section 2 reviews previously proposed model representations of iceberg capsizing. These rolling criteria assume that an iceberg will roll once a critical width-to-height ratio has been crossed. However, previous studies disagree on the value of this ratio.

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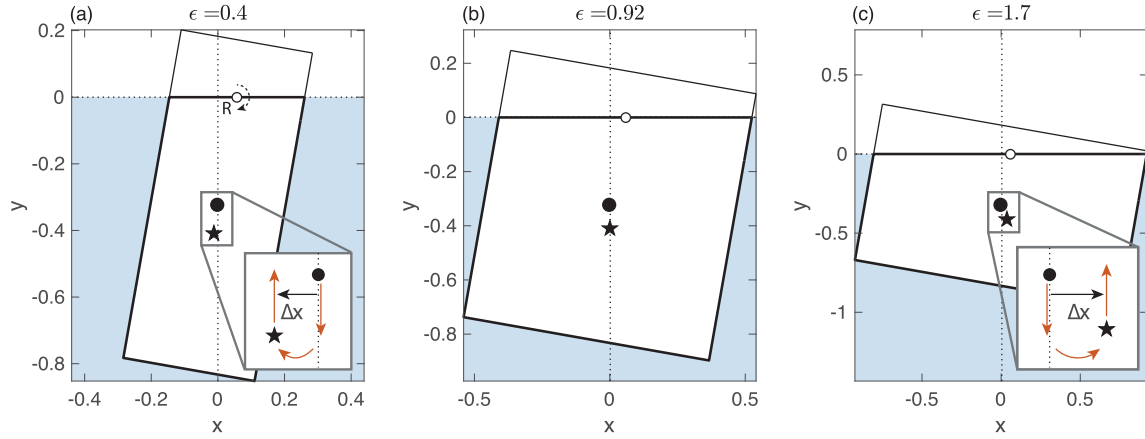


Fig. 1. Schematics of free-floating icebergs with various aspect ratios, $\epsilon \equiv W/H$. Here, $\alpha = 0.83$ and $\theta = 10^\circ$. Shown are the center of gravity (●), the center of buoyancy (★), and the point of rotation R (○). (a) $\epsilon = 0.4$, with $\Delta x < 0$, giving an unstable iceberg that will roll over. (b) Marginally unstable iceberg with $\epsilon = \epsilon_c = 0.92$. In the present case, with $\theta = 10^\circ$, $\Delta x(\epsilon_c) = 0$. (c) Stable, self-righting iceberg, with $\epsilon = 1.7$ and $\Delta x > 0$. Insets indicate the horizontal shift of the center of buoyancy, Δx . The red arrows illustrate gravity, buoyancy and resulting torque (insets). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Section 3 investigates how rolling impacts the evolution of individual iceberg geometries and their overall lifespan, compared to simulations with icebergs undergoing no rolling. In **Section 4**, we consider the effect of rolling in a global climate model, focusing on iceberg meltwater distributions at the ocean surface. Conclusions are given in **Section 5**.

2. Rolling criteria

In what follows, we idealize icebergs to be cuboids, allowing us to consider their stability from a 2D cross-sectional perspective. Icebergs roll along the long axis, L , swapping height, H , and width, W . We further assume that icebergs are always in isostatic equilibrium and of uniform ice density, ρ_i . We define the density ratio $\alpha \equiv \rho_i/\rho_w$, where ρ_w is the density of water.

We will show that an iceberg is subject to rolling under infinitesimal perturbations when its width-to-height ratio, $\epsilon \equiv W/H$, is smaller than a given critical value, ϵ_c . For $\epsilon > \epsilon_c$, on the other hand, the iceberg will return to its original position following an infinitesimal perturbation.

An expression for ϵ_c was previously derived by MacAyeal et al. (2003), who evaluated the change in gravitational potential energy under small rotations for an ice-shelf fragment wedged between two segments of an ice shelf. This derivation was later applied to free floating icebergs by Burton et al. (2012), who performed laboratory experiments to test the criterion.

Here, we present an alternative derivation of ϵ_c by considering the torques acting on an iceberg after it is rotated: for a given clockwise rotation, θ , around point R (Fig. 1), the center of buoyancy of the submerged part of the iceberg will shift horizontally by a distance Δx relative to the center of gravity. It can be shown trigonometrically that this horizontal shift is

$$\Delta x = \frac{H}{2} \left[\left(\alpha - 1 + \frac{\epsilon^2}{12\alpha} \right) \sin \theta + \frac{\epsilon^2}{12\alpha} \sec \theta \tan \theta \right] \quad (1)$$

(see derivation in the Supplementary Information). Note that Eq. (1) holds only in the range of θ for which the top surface of the iceberg remains entirely above sea level, $0 \leq \theta < \tan^{-1}(2(1-\alpha)/\epsilon)$.

If $\Delta x > 0$, the counter-clockwise torque that results from the offset of the downward acting gravitational force and the upward acting buoyancy force opposes the direction of rotation, and it acts to restore the original equilibrium. This is the case for shallow wide icebergs (i.e., large ϵ), where we can approximately neglect

horizontal motion due to rotation and consider only that the left side is raised and the right side is lowered, leading to additional submerged ice to the right of the center of gravity (Fig. 1(c)). When $\Delta x < 0$, on the other hand, this torque acts in the direction of rotation, and the iceberg becomes unstable (Fig. 1(a)). This is the case for tall narrow icebergs (i.e., small ϵ), where we can approximately neglect vertical motion due to rotation and consider only that the top half is shifted right and bottom half is shifted left, leading to additional submerged ice to the left of the center of gravity.

We are interested in the response of the iceberg to infinitesimal perturbations, that is, for $\theta \rightarrow 0$. We compute the Taylor series of Eq. (1) for θ around zero, which gives

$$\Delta x = \frac{H}{2} \left(\alpha - 1 + \frac{\epsilon^2}{6\alpha} \right) \theta + \mathcal{O}(\theta^2). \quad (2)$$

The critical width-to-height ratio at which the iceberg becomes unstable under small perturbations can then be defined as $\epsilon_c \equiv \epsilon$ when $\Delta x = 0$ and $\theta \rightarrow 0$. From Eq. (2), we find

$$\epsilon_c = \sqrt{6\alpha(1-\alpha)}. \quad (3)$$

Note that under finite perturbations θ , icebergs with aspect ratios larger than ϵ_c may become unstable and capsize (MacAyeal et al., 2003; Burton et al., 2012).

An iceberg rolling criterion that is widely used in current iceberg models was introduced by Weeks and Mellor (1978) (henceforth, WM78). WM78 derived a rolling criterion using insights from the ship-building literature (see Supplementary Information), leading to an expression similar to (3). However, WM78 further accounted for an increase in ice density with depth by introducing a correction height, Δ . In this case, it can be shown that the rolling criterion should become

$$\epsilon_c = \sqrt{6\alpha(1-\alpha) - 12\alpha \frac{\Delta}{H}}. \quad (4)$$

(A derivation of criterion (4) is provided in the Supplementary Information.) In agreement with physical intuition, the increase in density with depth leads to a lower value of ϵ_c . However, we find that the derivation in WM78 erroneously replaced Δ with $-\Delta$ in the stability criterion [see their equation (9)], an error that does not appear to have been noted in the literature previously and has been carried in many subsequent studies, as discussed below.

WM78 estimated the effective mean density ratio to be $\alpha = 0.81$. By substituting $\alpha = 0.81$ into (4) and replacing Δ with $-\Delta$, we find that the sign error in Δ leads to $\epsilon_c > 1$ for $H < 730$ m.

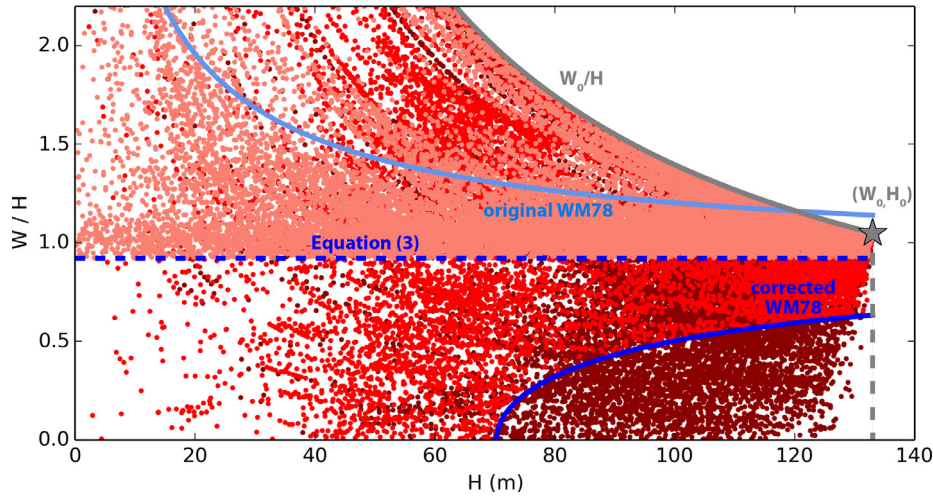


Fig. 2. Different rolling criteria, $\epsilon_c(H)$ (blue lines) and simulated iceberg width-to-height ratios (dots). Rolling occurs when W/H for a given iceberg falls below a given blue line. The criterion of WM78 is indicated (light blue), along with a version in which the sign error is corrected (dark blue). Note that here $\alpha = 0.83$, which implies that the corrected WM78 criterion reaches zero when $H \approx 71$ m. Also shown is the criterion of Eq. (3) (dashed blue). Note that any criterion with $\epsilon_c > 1$ leads to continuous rolling. Width-to-height ratios are indicated for medium-sized icebergs [size class 3 from Stern et al. (2016)] from GCM model runs with different rolling criteria: non-rolling icebergs (dark red), rolling according to the corrected WM78 scheme (red), and rolling according to Eq. (3) (light red). Two years from the simulations are shown, with iceberg dimensions sampled monthly. The original dimensions (W_0, H_0) for all icebergs are indicated by the gray star. Icebergs that fall on the solid gray boundary line experience no side melt and only basal melt (i.e., $W/H = W_0/H_0$). The gray dashed vertical line indicates the limit of pure side melt ($W/H = W/H_0$). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Among other issues, this has the unphysical consequence that all icebergs with $H < 730$ m will continuously roll once ϵ falls below ϵ_c . In other words, once the 200 m thick icebergs considered in WM78 capsize for the first time, they will continue to roll at each model time step.

WM78 were primarily concerned with an idealized iceberg of thickness $H = 200$ m, and they approximated the center of gravity correction to be constant, with $\Delta = 6$ m. It should be emphasized that even the corrected WM78 formulation is not appropriate for use in the continuous evolution of a decaying iceberg. First, when the iceberg thickness changes, Δ should evolve rather than being held constant. This issue is especially egregious for small icebergs, where $\Delta = 6$ m places the center of gravity of the iceberg so low that the iceberg is unconditionally stable. A consequence of this is that ϵ_c is no longer defined when $H < 12\Delta/6(1 - \alpha) \approx 63$ m (for the values used in WM78), and icebergs no longer roll in model simulations, which allows narrow, pin-like icebergs to occur (Fig. 2). Second, the density profile of the iceberg assumed in the WM78 derivation (i.e., that icebergs are densest near the bottom) would be rotated by 90° upon the first instance of rolling, rendering Eq. (4) no longer appropriate.

However, the criterion of WM78 has been adopted by many studies of continuous iceberg evolution, which have applied the criterion under a broad range of iceberg dimensions. For example, the rolling criterion (including the sign error and constant value of Δ) is adopted in the seminal study of Bigg et al. (1997), who consider icebergs of 10 different size classes ranging from $100\text{ m} \times 66\text{ m} \times 80\text{ m}$ to $1500\text{ m} \times 1000\text{ m} \times 360\text{ m}$. In addition to adopting the sign error from WM78, the model of Bigg et al. (1997) also erroneously takes the critical threshold to apply to the ratio L/H rather than W/H . In other words, the horizontal length dimension that is used for the rolling criterion is not the same as the dimension that is rotated from horizontal to vertical when the iceberg rolls. All of these errors – the sign error in Δ , the constant value of Δ associated with $H = 200$ m being applied to a wide range of iceberg thicknesses, and the threshold applying to L/H – are adopted in the more recent iceberg modeling studies of Gladstone et al. (2001), Jongma et al. (2009), and Martin and Adcroft (2010). Martin and Adcroft (2010) furthermore erroneously replace H with the draft αH in their representation of the rolling criterion (4). The

model of Bigg et al. (1997) has been widely adopted, and many recent iceberg modeling studies include these errors in the rolling scheme (e.g., Death et al., 2006; Levine and Bigg, 2008; Wiersma and Jongma, 2010; Jongma et al., 2013; Death et al., 2014; Roberts et al., 2014; vanden Berk and Drijfhout, 2014; Bügelmayr et al., 2015; Marsh et al., 2015; Merino et al., 2016; Stern et al., 2016).

In order to take into account the varying density profile of an iceberg, a more complete theory of the density evolution of the iceberg would have to be developed. However, the constant density criterion in Eq. (3) may provide a sufficiently accurate approximation for many purposes.

Based on observed ice-shelf densities from Larsen A and B, MacAyeal et al. (2003) estimated $\epsilon_c \approx 0.8$, which is close to the value of WM78 and subsequent studies, while Burton et al. (2012) use $\epsilon_c = 0.75$. In the following, we take $\rho_i = 850\text{ kg/m}^3$ (Silva et al., 2006) and $\rho_w = 1025\text{ kg/m}^3$, such that $\alpha = 0.83$ (Martin and Adcroft, 2010; Stern et al., 2016), which gives $\epsilon_c \approx 0.92$. Note that this value of ρ_i is lower than for pure ice due to factors including the snow and firn in the iceberg not being fully compacted. The stability criterion from Eq. (3), as well as the original and corrected WM78 schemes, are illustrated in Fig. 2.

3. Impact of rolling on individual icebergs

In order to study the impact that rolling has on individual icebergs, we will compare two scenarios: (i) icebergs undergoing no rolling and (ii) icebergs that roll according to the scheme in Eq. (3). We eschew the WM78 scheme in this section in light of the issues raised above. We briefly revisit the WM78 scheme for the GCM simulations in Section 4 in order to estimate the potential bias that the errors in this scheme may have introduced in previous studies.

3.1. Iceberg decay model

We first summarize the widely used decay representation by Martin and Adcroft (2010), which is based on the earlier work by Bigg et al. (1997). In this formulation, only three melt processes are considered: (i) wind-driven wave erosion, M_e ; (ii) turbulent basal melt, M_b ; and (iii) side wall erosion from buoyant convection, M_v . Other processes, such as top and bottom surface melt,

are typically small compared to these (Savage, 2001). The iceberg dimensions evolve according to $dL/dt = dW/dt = M_e + M_v$ and $dH/dt = M_b$, with iceberg volume given by $V = LWH$. The individual decay terms are written as follows (Martin and Adcroft, 2010; Wagner and Eisenman, 2017):

$$M_e = \frac{1}{2} (1 + \cos[\pi A_i^3]) (p_1 + p_2 T_w) S(\bar{v}_a, \bar{v}_w), \quad (5)$$

$$M_v = b_1 T_w + b_2 T_w^2,$$

$$M_b = c |\bar{v}_w - \bar{v}_i|^{0.8} (T_w - T_i) L^{-0.2},$$

where A_i is the fractional sea ice cover, $p_1 = 0.67$, $p_2 = 0.33^\circ\text{C}^{-1}$, and T_w is the SST in $^\circ\text{C}$. Sidewall erosion is set to $M_v = 0$ if $T_w < 0^\circ\text{C}$. Here, $S = a_1 |\bar{v}_a - \bar{v}_w|^{1/2} + a_2 |\bar{v}_a - \bar{v}_w|$ is related to the sea state (Martin and Adcroft, 2010), with $a_1 = 8.7 \times 10^{-6} \text{ m}^{1/2} \text{ s}^{-1/2}$ and $a_2 = 5.8 \times 10^{-7}$. Furthermore, $b_1 = 8.8 \times 10^{-8} \text{ m s}^{-1} \text{ }^\circ\text{C}^{-1}$, $b_2 = 1.5 \times 10^{-8} \text{ m s}^{-1} \text{ }^\circ\text{C}^{-2}$, $c = 6.7 \times 10^{-6} \text{ m}^{-2/5} \text{ s}^{-1/5} \text{ }^\circ\text{C}^{-1}$, and T_i is the temperature of the ice which is taken to be fixed at -4°C .

3.2. Rolling under constant forcing

In order to estimate how rolling impacts the evolution of the iceberg, it is useful to first consider average forcing conditions. From the GCM simulations of Section 4 we find that average speeds experienced by present-day icebergs are approximately $|\bar{v}_a| = 3 \text{ m/s}$, $|\bar{v}_w| = 0.04 \text{ m/s}$, and $|\bar{v}_i| = 0.06 \text{ m/s}$, and average SSTs are approximately $T_w = -1.2^\circ\text{C}$. This low temperature value is largely due to the simulated present-day icebergs spending a large fraction of their life surrounded by sea ice (average $A_i = 0.75$). For these average forcing values, we obtain $M_e \sim 0.3 \text{ m/d}$, $M_b \sim 0.06 \text{ m/d}$, and $M_v \sim 0.004 \text{ m/d}$. Note that the dominance of the wind-driven wave erosion term is in agreement with previous findings (e.g., Gladstone et al., 2001). The evolution of the individual dimensions of a non-rolling and a rolling iceberg are illustrated in Fig. 3(a) and (b), using the melt rates above and ignoring the effects of iceberg drift. The figure shows that rolling slows down an iceberg's melt. The reason for this is that for all realistic values of α , the critical ratio satisfies $\epsilon_c < 1$, i.e., $W < H$ at the time of rolling. This implies that the surface area of the sidewalls, $A = 2H(W + L)$, decreases when the iceberg rolls (because H and W are swapped). As a consequence, the rate of volume loss decreases once rolling begins (Fig. 3(c)), since $dV/dt \approx -AM_e/2$ (neglecting the typically smaller terms M_b and M_v).

3.2.1. Onset of rolling. As a first step, we set $M_v = M_b = 0$, since both terms are typically considerably smaller than M_e . In this approximation, H remains constant. For given initial iceberg dimensions, H_0, W_0, L_0 , the critical width at which icebergs roll for the first time is then $W_r = \epsilon_c H_0$. Taking $L_0/W_0 = 3/2$, as is often done in current iceberg models, we find $L_r = (1/2 + \epsilon_c/\epsilon_0)W_0$, where $\epsilon_0 \equiv W_0/H_0$. The volume fraction at first rolling is then

$$V_r/V_0 = \frac{1}{3} (1 + 2\epsilon_c/\epsilon_0) (\epsilon_c/\epsilon_0). \quad (6)$$

In order to study the onset of rolling for different initial iceberg sizes, we consider 10 commonly used iceberg size classes, ranging in dimensions from $60 \times 40 \times 40 \text{ m}$ to $2200 \times 1467 \times 250 \text{ m}$ (Table 1). For size classes 1–3, $\epsilon_0 = 1$ and Eq. (6) gives $V_r/V_0 = 0.87$, i.e., the iceberg will roll for the first time once it is 13% decayed. For size classes 4–10, ϵ_0 increases, which leads to a decrease in V_r/V_0 . Fig. 3(d) summarizes how V_r/V_0 varies with size class, showing the analytical upper limit (6), as well as values that take into account nonzero values of M_v and M_b . For size class 10, the iceberg begins to roll when it is 98% decayed (considering all three melt terms). This highlights that iceberg rolling is most significant for small icebergs.

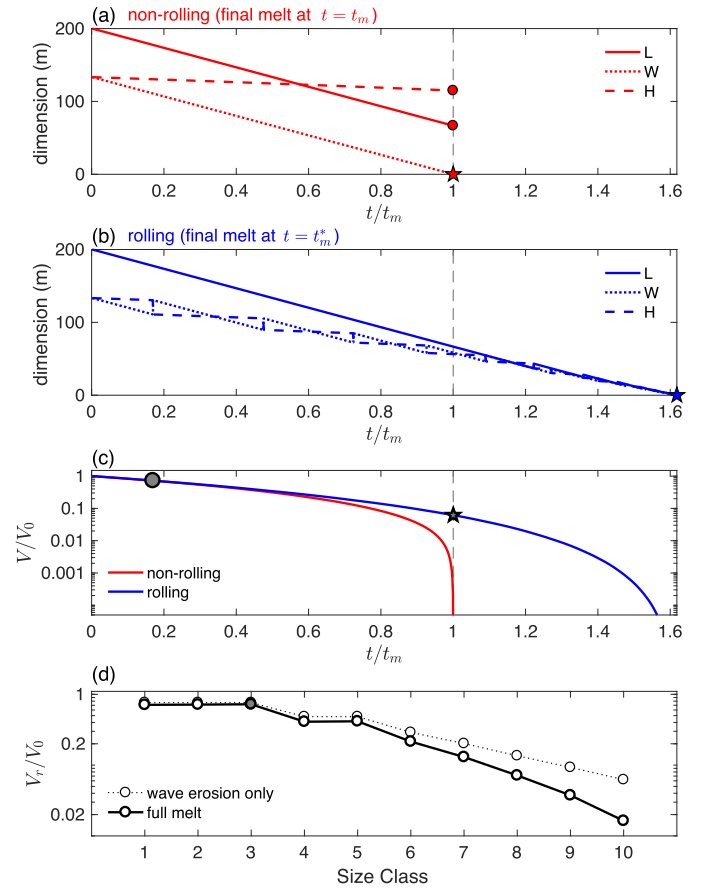


Fig. 3. Evolution of iceberg dimensions and volume in simulations with constant forcing. (a) Decay of a non-rolling iceberg of size class 3 using constant forcing values. Shown are dimensions L (solid), W (dotted), and H (dashed) versus time (scaled by time of final melt, t_m). The iceberg has fully melted when $W = 0$ (star). Unphysically, L and H have not reached zero (circles). (b) As in panel a, but including iceberg rolling. Note that here all dimensions reach zero at the same time, t_m^* (star). (c) Volume scaled by initial volume corresponding to panels a and b. Symbols are included to indicate the volume at the time of initial roll (circle), as well as the remaining volume of the rolling iceberg when the non-rolling iceberg has melted (star). (d) Volume (scaled by initial volume) at the time of initial roll for the 10 size classes of Table 1. The dotted line corresponds to the analytical upper limit of Eq. (6), which takes $M_v = M_b = 0$. The gray circle corresponds to the gray circle in panel c.

Table 1

Initial iceberg dimensions and $\epsilon_0 \equiv W_0/H_0$ for the 10 size classes used here (adapted from Stern et al. (2016), which is based on Gladstone et al. (2001)).

Size Class	L_0 (m)	W_0 (m)	H_0 (m)	ϵ_0
1	60	40	40	1
2	100	67	67	1
3	200	133	133	1
4	350	233	175	1.3
5	500	333	250	1.3
6	700	467	250	1.9
7	900	600	250	2.5
8	1200	800	250	3.2
9	1600	1067	250	4.3
10	2200	1467	250	5.9

3.2.2. Impact of rolling on iceberg life span. Under the approximation that $M_b = M_v = 0$, a non-rolling iceberg would completely melt at time $t_m = W_0/M_e$, regardless of L_0 . The time of complete melt for a rolling iceberg, on the other hand, can be readily shown to be

$$t_m^* = [5/4 + 1/(2\epsilon_0)](W_0/M_e), \quad (7)$$

where we again have fixed $L_0/W_0 = 3/2$. The relative life span of rolling versus non-rolling icebergs is then $t_m^*/t_m = 5/4 + 1/(2\epsilon_0) > 1$,

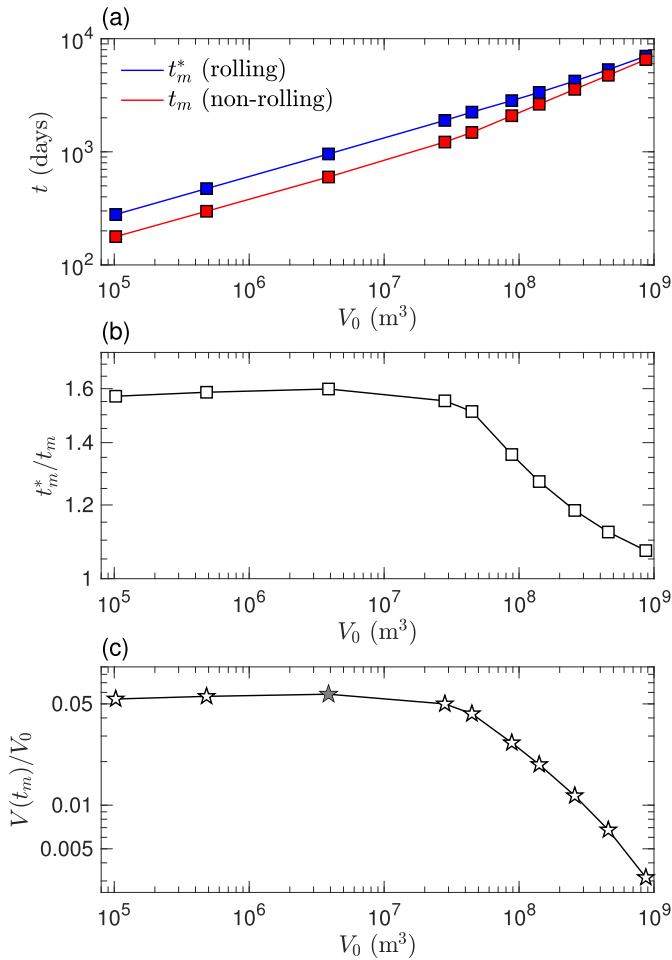


Fig. 4. Iceberg life spans in simulations with constant forcing. (a) Duration of iceberg life as a function of initial iceberg size, for size classes 1–10 (see text). (b) Ratio of iceberg lifespans with and without rolling, t_m^*/t_m , which shows that rolling icebergs of size classes 1–5 have lifespans about 60% longer than non-rolling icebergs. For large icebergs, L is sufficiently large that it does not reach zero when W and H have fully melted. This results in a reduction of t_m^*/t_m for large V_0 . (c) Fraction of the volume of the rolling iceberg that remains at the time when the non-rolling iceberg disappears, $V(t_m)/V_0$. The gray star corresponds to the scenario in Fig. 3(a)–(c).

i.e., rolling icebergs always live longer (Fig. 4(a)). Icebergs with a large initial width-to-height ratio, such that $\epsilon_0 \rightarrow \infty$, live 25% longer. Icebergs in size classes 1–3 (with $\epsilon_0 = 1$) live 75% longer due to rolling. Fig. 4(b) shows that, by accounting for M_b and M_v , the actual increase in life span due to rolling for size classes 1–5 is closer to 60%.

Note that Eq. (7) assumes constant forcing and neglects the impact of rolling on drift dynamics, which can also impact melt rates (see Section 4). Fig. 4(b) shows that t_m^*/t_m decreases rapidly for large icebergs. For size classes 7–10, t_m^*/t_m falls below the limit $5/4$, which is due to W and H reaching zero before L has melted completely. This highlights an unphysical feature in many current iceberg models: the models ultimately end up with long, infinitesimally thin icebergs. Finally, even though rolling icebergs can live substantially longer than non-rolling icebergs, the remaining volume at time t_m (when the non-rolling iceberg has completely melted) is small, with $V(t_m)/V_0 < 6\%$ (Fig. 4(c)).

4. Impact of rolling in iceberg–climate model simulations

In what follows we compare the meltwater release in model simulations with rolling and non-rolling icebergs, using (1) an ide-

alized iceberg drift and decay model and (2) a comprehensive coupled GCM.

4.1. Idealized offline iceberg model

We use a recently developed drift model which evolves iceberg velocity under the influence of air drag, water drag, the pressure gradient force, and the Coriolis force (Wagner et al., 2017). This formulation is somewhat idealized compared to previous iceberg models (e.g., Bigg et al., 1997; Gladstone et al., 2001; Marsh et al., 2015), allowing an analytical solution for iceberg velocity as a function of surface air and water velocities. The model operates in an offline mode, meaning that the iceberg trajectories are computed as non-interactive Lagrangian particles, using precomputed input surface velocity and SST fields. This allows for a rapid integration of large numbers of iceberg trajectories. The drift model is coupled to the decay model of Eq. (5).

The precomputed input fields are taken from NASA’s Estimating the Circulation and Climate of the Ocean Phase II (ECCO2) global ocean state estimate (Menemenlis et al., 2008). We perform two sets of simulations, one with iceberg rolling using the scheme in Eq. (3) and one without iceberg rolling. In order to avoid canceling effects due to different iceberg release locations (see Section 4.2), we initialize icebergs in a small region just off the coast of Sermiilik Fjord, East Greenland, into which Helheim Glacier, one of Greenland’s largest outlet glaciers, drains (green star in Fig. 5(a)). The release location of each iceberg is set to be at the center of a grid box which is randomly chosen from a 5×4 region of grid boxes. Since this region only has substantial sea ice for a brief period of the year, we set the sea ice concentration to zero in the following simulations.

We release 5000 icebergs of each of the 10 iceberg size classes specified in Stern et al. (2016), at a rate of approximately 14/day, over the input year 1992. Icebergs are released at identical locations and times in the two simulations, and they are tracked until fully decayed.

Fig. 5 illustrates the results for size class 5, which are approximately representative of the other size classes (not shown). The longer life span and farther reach of rolling icebergs that are expected from the results of Section 3 are readily seen in these simulations. The blue and red dots in Fig. 5(a) show the final melting points of rolling and non-rolling icebergs, respectively. The non-rolling icebergs are found to typically melt closer to the release location compared to the rolling icebergs. Fig. 5(b)–(f) illustrates the evolution of a representative pair of rolling and non-rolling trajectories. The rolling iceberg survives $\sim 20\%$ longer (Fig. 5(c)). The slow rate of decay over the first half of the icebergs’ lives (Fig. 5(c)–(e)) is due to cold winter conditions, and the melt rates speed up substantially during summer when the temperatures rise (Fig. 5(f)). Fig. 5(d) and (e) illustrate that the evolution of the simulated iceberg dimensions is comparable to that of the analytical version (Fig. 3(a) and (b)). The shorter relative life span of the rolling iceberg ($t_m^*/t_m = 1.2$), compared to the analytical value ($t_m^*/t_m \simeq 1.5$ in Fig. 4(b)), is likely due to a number of factors, including higher values of M_e once the iceberg reaches the warmer temperatures of the open ocean (Fig. 5(f)). Note that the rolling also has an immediate effect on the iceberg’s drift direction. This is due to rolling changing the aspect ratio of the iceberg, and hence changing the momentum balance. This explains why the iceberg trajectories diverge upon the first rolling event ($t = 161$ d), long before the final melt of the non-rolling iceberg ($t = 228$ d, Fig. 5(b)). Furthermore, the change in aspect ratio from rolling causes the iceberg drift to slow (not shown), which reduces the spread of the rolling icebergs. This slowdown is a consequence of the horizontal iceberg surface area increasing when it rolls: iceberg drift velocities are dependent

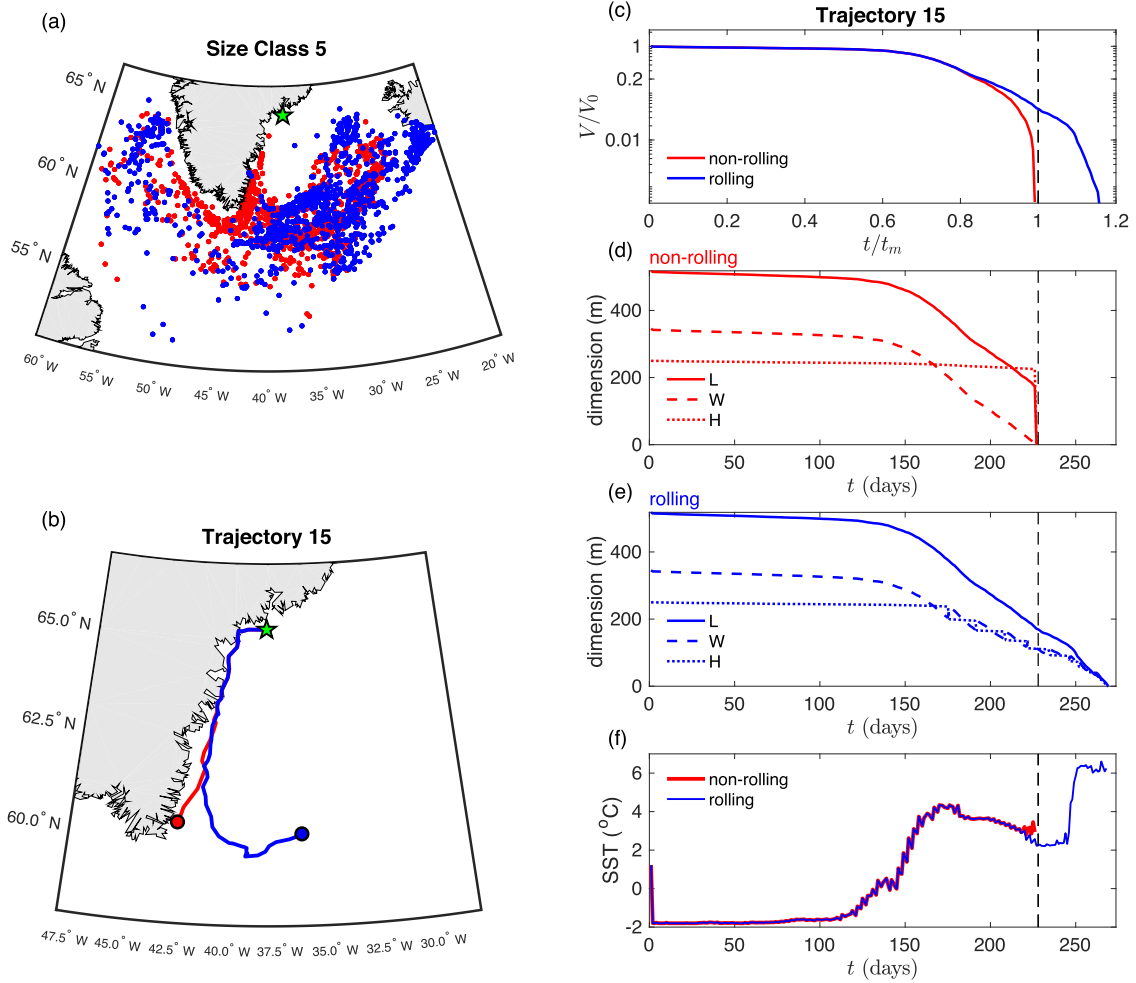


Fig. 5. Results from the idealized offline iceberg simulations of Section 4.1. (a) Locations of final melt for size class 5 rolling icebergs (blue) and non-rolling icebergs (red). All icebergs are released from the region marked by the green star (near the mouth of Sermilik Fjord, East Greenland). (b) Detail of a pair of rolling and non-rolling iceberg trajectories. (c) Evolution of volume (scaled by initial volume), corresponding to this pair of trajectories. The time of complete melt of the non-rolling iceberg, $t = t_m$, is indicated (dashed black). (d) Evolution of iceberg dimensions for this non-rolling trajectory, and (e) for this rolling trajectory. (f) SST conditions experienced by these two icebergs. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

on the horizontal surface area, with larger surface area reducing drift velocities (Wagner et al., 2017).

In order to assess the level of large-scale impacts of iceberg rolling, we consider simulations with a coupled GCM in the next section. This allows us to address the question whether the biases shown in Fig. 5(a) are substantial in comprehensive model runs, or whether they are small compared to the internal variability of the system.

4.2. GCM Simulations

We use the Geophysical Fluid Dynamics Laboratory (GFDL) coupled climate model CM2G (Delworth et al., 2006; Cooke et al., 2012), which includes the following components: AM2 atmosphere model, MOM6 ocean model, SIS2 sea-ice model, and LM3 land model, as well as the iceberg component detailed in Martin and Adcroft (2010). The ocean model uses a $1^\circ \times 1^\circ$ horizontal grid, with 63 isopycnal layers in the vertical, and the atmospheric model has a 2° horizontal resolution. The model setup is as described in Stern et al. (2016), except for the iceberg rolling scheme. The icebergs in these simulations are fully coupled to the climate model, so that the melt water from the icebergs freshens and cools the ocean surface, which can lead to feedbacks in the climate system.

Icebergs are released into the global ocean according to the scheme of Stern et al. (2016), using the same 10 iceberg size

classes, size class distributions, and release locations. CM2G computes iceberg calving fluxes by routing excess frozen precipitation over the ice sheets instantaneously to the coastline via hydraulic potential pathways. These locations encompass most major ice shelves and outlet glaciers in the Arctic and Antarctic. The simulations are run for 150 years each.

We perform three simulations: one with iceberg rolling using the scheme in Eq. (3), one with rolling using the WM78 scheme but with the error in the sign of Δ corrected, and one with no iceberg rolling. Icebergs in these simulations fill the phase space of available aspect ratios (W/H), bounded by the critical rolling ratio ϵ_c and the limits W_0/H and W/H_0 (see Fig. 2). The latter two limits indicate pure basal melt and pure sidewall melt, respectively. The large spread of simulated ratios in Fig. 2 indicates the wide range of ocean conditions and melt rates experienced by icebergs in different parts of the globe and at different times of the year.

Rolling is expected to have the greatest impact in the simulations that use Eq. (3), because rolling occurs much earlier than in those using the corrected WM78 scheme. Hence the following focuses on comparing simulations with non-rolling icebergs and icebergs that roll according to Eq. (3).

Fig. 6(a) and (b) show the freshwater flux due to iceberg melting around Antarctica and Greenland, averaged over the final 100 years of the simulations with the scheme from Eq. (3). These distributions are qualitatively similar to those in previous studies (e.g.,

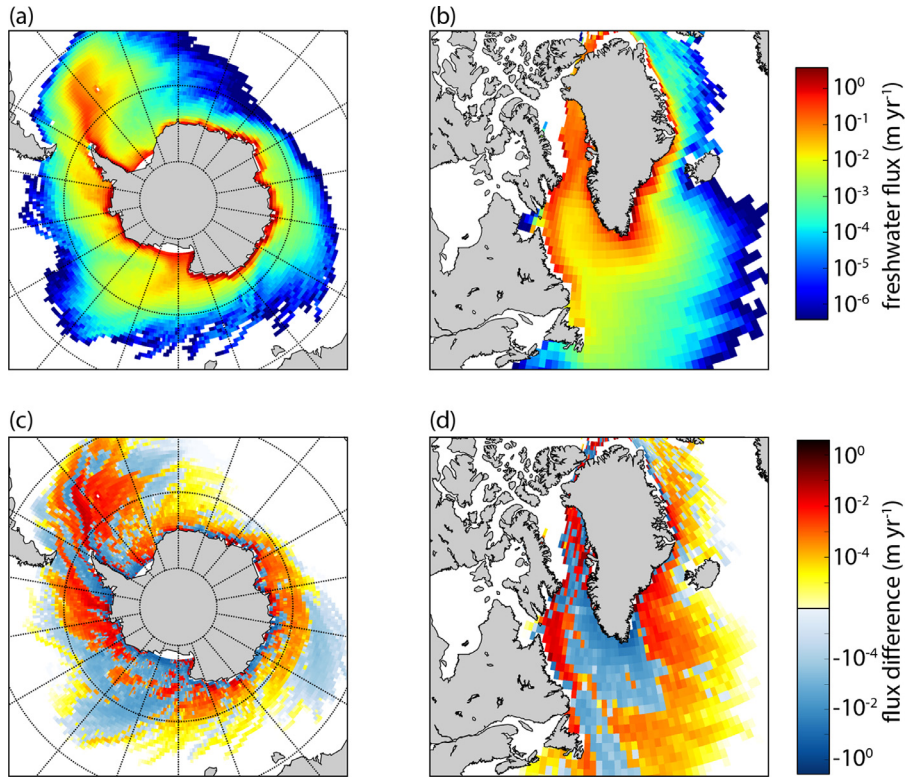


Fig. 6. GCM freshwater fluxes. (a) Antarctic freshwater flux from iceberg melt, averaged over 100 years, using the iceberg rolling scheme of Eq. (3). (b) As in panel (a) but for Greenland. (c) and (d) Differences in freshwater flux, calculated from the simulations with iceberg rolling (a,b) minus those without rolling (not shown). No regions show statistically significant differences. All fluxes are given in meters per year on a logarithmic scale.

Martin and Adcroft, 2010; Stern et al., 2016, who used the original WM78 scheme), which indicates that the differences in rolling schemes do not dramatically affect the large-scale freshwater flux distribution. This point is further supported when we compute the difference in freshwater flux between the rolling and non-rolling simulations in Fig. 6(c) and (d). The most notable differences in the Antarctic simulations are a slight increase of meltwater for rolling icebergs north of the Antarctic peninsula and a decrease around the peninsula's coast. This suggests that rolling allows icebergs to transport meltwater further offshore, in agreement with the findings of the previous section. A similar mechanism might be inferred from the differences around Greenland, where meltwater decrease near the southern tip of Greenland and a small increase off the Labrador coast suggests that rolling icebergs are transported further along the Greenland coastal currents. However, none of these differences are statistically significant at the 95% confidence level over the time period of integration. The same result is found for simulations with the corrected WM78 scheme (not shown). The relatively small influence of rolling appears to be due to (i) the high level of internal variability of the overall freshwater forcing (which is strongly influenced by factors including the presence of sea ice which itself is highly variable), and (ii) the fact that rolling affects icebergs only after much of their initial volume has already melted, as discussed above (Fig. 3).

The small differences in the overall freshwater flux do not rule out that rolling icebergs may on average live longer or travel farther than their non-rolling counterparts, as may be expected from Sections 2 and 3. However, the wide range of ocean conditions which icebergs experience, together with the large internal variability in the coupled climate model, give rise to a large spread of iceberg lifetimes (Fig. 7). Modeled iceberg lifetimes are, for example, sensitive to sea ice conditions, and can be greatly increased by icebergs becoming stuck along the Antarctic and Greenlandic

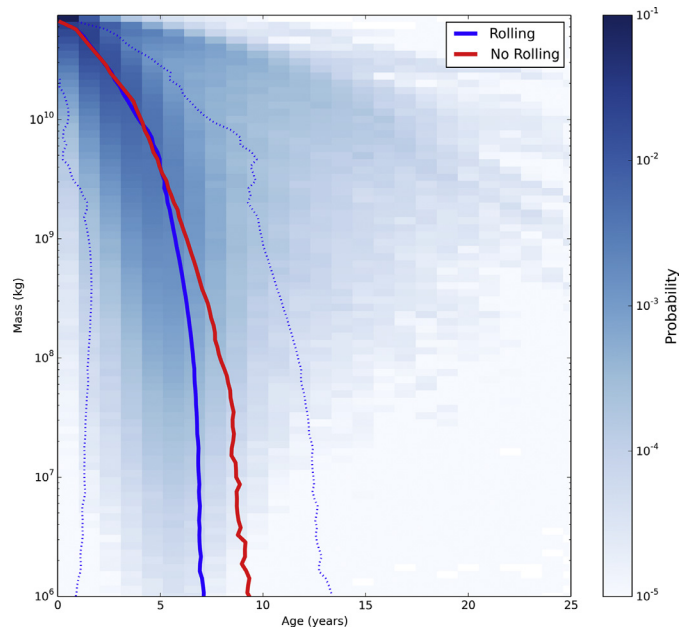


Fig. 7. Evolution of iceberg mass from GCM simulations for size class 10 (considering all icebergs in the global simulations). Shading shows relative probabilities of iceberg mass as a function of iceberg age for rolling icebergs, using the rolling scheme of Eq. (3). The corresponding probabilities for non-rolling icebergs (not shown) are qualitatively similar. Lines indicate the mean rolling (solid blue) and non-rolling (red) iceberg masses over time, as well as the spread of the rolling icebergs (dotted blue lines indicating one standard deviation about the mean). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

coasts (factors that are not taken into account in the idealized model of Section 4.1). Furthermore, in the Northern Hemisphere icebergs decay more slowly if they drift into the central Arctic basin. Differences between Northern and Southern Hemisphere lifetimes are illustrated in Fig. S3.

We find that in the GCM non-rolling icebergs live on average slightly longer than their rolling counterparts (contrary to the idealized model results of Sections 3.2 and 4.1), although Fig. 7 shows that this difference is small compared to the spread of simulated iceberg lifetimes. This slightly counter-intuitive result may be due to several factors: First, the high level of internal variability and long time scales of the coupled climate system result in different sea ice conditions for the two simulations, especially in the Northern Hemisphere (not shown). While these differences are not statistically significant when averaged over the 150 year simulation period, we do overall observe slightly warmer surface temperatures (and decreased sea ice) in the rolling simulation, which leads to more rapidly decaying icebergs. In addition to internal variability, iceberg lifetimes are influenced by their trajectories, as discussed above. After rolling, icebergs tend to spread more readily away from the coast (both in Antarctica and Greenland, see also Fig. 5(a)), causing them to be exposed to warmer waters. The combination of warmer conditions in the rolling simulation and more offshore trajectories for rolling icebergs appear to be sufficient to offset the decreases in iceberg decay caused by the geometric considerations of Section 3.

In summary, the findings of this section suggest that the large-scale biases that are introduced in coupled climate simulations by the differences between these iceberg rolling schemes are relatively small.

5. Conclusion

In this study, we have addressed how to account for iceberg capsizing in models that explicitly represent icebergs. We have shown that a widely used rollover criterion, based on the work of Weeks and Mellor (1978), is not suitable to describe the rolling of icebergs for a typical range of iceberg sizes. The results presented here suggest that this criterion should be replaced by the more physical scheme in Eq. (3). For studies concerned with the detailed simulation of individual iceberg trajectories, however, a more sophisticated rolling scheme may be required.

We have found that rolling can substantially impact the drift and decay of individual icebergs, especially those that are relatively small (length $\lesssim 500$ m). For example, we find that for fixed surface velocities and SSTs, rolling icebergs typically live substantially longer and drift farther than non-rolling icebergs. This suggests that in regions where more small icebergs calve off glaciers or ice shelves, capsizing may have a large impact on meltwater fluxes. Hence the results presented here may be relevant to both operational iceberg forecast models and regional climate model simulations. Nonetheless, we have shown that iceberg rolling has a relatively small impact on the large-scale iceberg meltwater flux in the global climate system.

Acknowledgments

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Supplementary material

Supplementary material associated with this article can be found in the online version at [10.1016/j.ocemod.2017.07.003](https://doi.org/10.1016/j.ocemod.2017.07.003).

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Supplementary Information for “On the representation of capsizing in iceberg models”

TILL J.W. WAGNER, ALON A. STERN, REBECCA W. DELL, AND IAN EISENMAN

Derivation of rolling stability criterion

Here we present a derivation of the iceberg rolling stability criterion, ϵ_c , by considering the torques acting on the iceberg after a given rotation, θ . Note that this is an alternative approach to the previous derivation by MacAyeal et al (2003), who minimized the potential energy of the system in order to find ϵ_c .

Consider the cross-section of a cuboid iceberg of height H and width W . The iceberg is taken to float at isostatic equilibrium, with densities of water ρ_w and ice ρ_i . For a given angle of rotation, θ , the horizontal position of the center of gravity, x_g , can be seen to be

$$x_g = -\left(D - \frac{H}{2}\right) \sin \theta = -H \left(\frac{\rho_i}{\rho_w} - \frac{1}{2} \right) \sin \theta, \quad (\text{S1})$$

(with the origin chosen to be located at the point of rotation, R , as indicated in Fig S1). Here $D \equiv (\rho_i/\rho_w)H$ is the draft of the iceberg, and $D - H/2$ is the distance between R and x_g (Fig. S1). The center of buoyancy, x_b , is readily derived by sectioning the submerged area of the iceberg into a triangle (a,b,c) with area A_1 and center of buoyancy horizontal coordinate x_1 and a rectangle (a,c,d,e) with area A_2 and center of buoyancy horizontal coordinate x_2 , as indicated in Fig S1:

$$x_b = \frac{x_1 A_1 + x_2 A_2}{A_1 + A_2}. \quad (\text{S2})$$

Note that this is only satisfied for $|\theta| < \tan^{-1} [2(1 - \rho_i/\rho_w)H/W]$, which is the angle for which the lowest point of the iceberg’s top surface is equal to the water surface.

The horizontal locations of the triangle vertices (x_a, x_b, x_c) can be seen to satisfy $x_a \cos \theta = -W/2$, $x_b \cos \theta = W/2$, and $x_c - x_a = W \cos \theta$. This implies that

$$x_1 = \frac{1}{3} (x_a + x_b + x_c) = \frac{1}{3} x_c = \frac{W}{3} \left(\cos \theta - \frac{1}{2 \cos \theta} \right). \quad (\text{S3})$$

The horizontal locations of the additional rectangle vertices (x_d, x_e) can be seen to satisfy $x_a - x_e = x_c - x_d = x' \equiv (D - \frac{W}{2} \tan \theta) \sin \theta$, which implies that

$$\begin{aligned} x_2 &= \frac{1}{4} (x_a + x_c + x_d + x_e) = \frac{1}{4} [x_a + x_c + (x_c - x') + (x_a - x')] \\ &= \frac{1}{2} (x_a + x_c - x') = \frac{1}{2} \left[-\frac{W}{\cos \theta} + W \cos \theta - (D - \frac{W}{2} \tan \theta) \sin \theta \right]. \end{aligned}$$

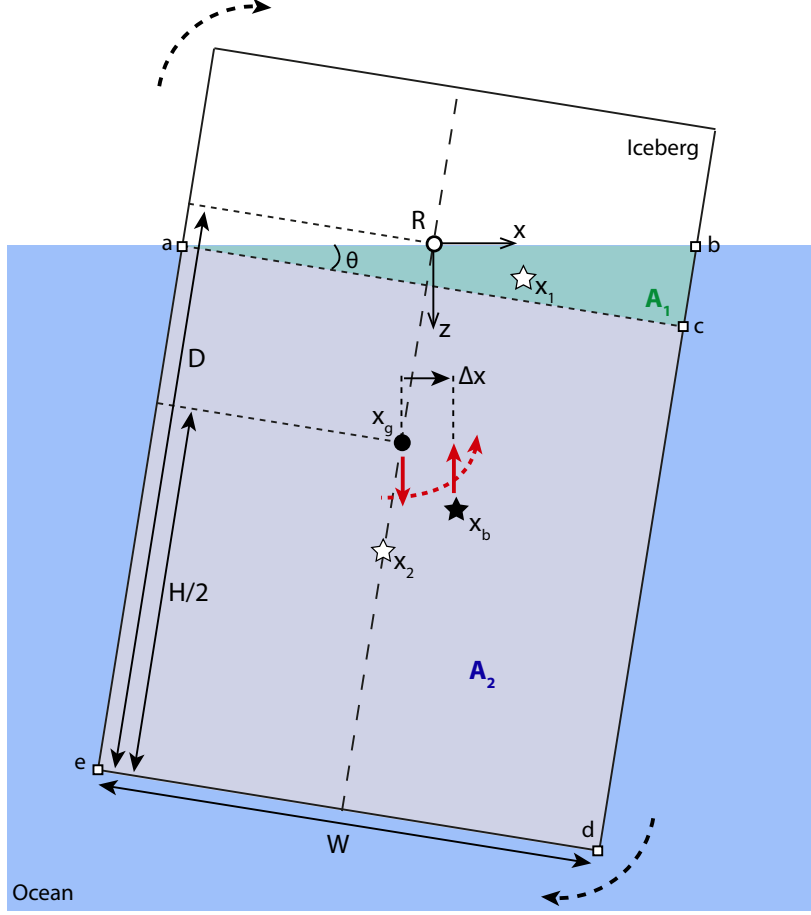


Figure S1. Schematic of an iceberg of width W and height H , rotated clockwise by an angle θ (defined to be positive in this schematic). The center of rotation is shown at point R (\circ). Indicated in blue and green are the two submerged areas, with auxiliary centers of buoyancy (\star) used to compute the overall center of buoyancy (\blackstar). Also shown is the center of gravity (\bullet), as well as the horizontal offset between the centers of buoyancy and gravity, $\Delta x = x_b - x_g$. The red arrows indicate the forces of gravity and buoyancy (solid) and the resulting torque (dashed). Since $\Delta x > 0$ in the case illustrated, the resulting torque counteracts the rotation θ , leading to a stable, self-righting, iceberg configuration.

Since $-1/\cos\theta + \cos\theta = (1/\cos\theta)(-1 + \cos^2\theta) = (1/\cos\theta)(-\sin^2\theta) = -\tan\theta \sin\theta$, this simplifies to

$$\begin{aligned}
 x_2 &= \frac{1}{2} \left[-W \tan\theta \sin\theta - \frac{\rho_i}{\rho_w} H \sin\theta + \frac{W}{2} \tan\theta \sin\theta \right] \\
 &= \frac{1}{2} \left[-\frac{W}{2} \tan\theta \sin\theta - \frac{\rho_i}{\rho_w} H \sin\theta \right] \\
 &= -\frac{1}{2} \sin\theta \left(\frac{\rho_i}{\rho_w} H + \frac{W}{2} \tan\theta \right). \tag{S4}
 \end{aligned}$$

Supplementary Information

The submerged areas can be seen to be

$$A_1 = \frac{1}{2}(W)(W \tan \theta) = \frac{1}{2}W^2 \tan \theta, \quad (\text{S5})$$

$$A_2 = (W)\left(D - \frac{1}{2}W \tan \theta\right) = \frac{\rho_i}{\rho_w}HW - \frac{1}{2}W^2 \tan \theta. \quad (\text{S6})$$

Note that the total submerged area is thus $A_1 + A_2 = (\rho_i/\rho_w)HW$. Substituting equations (S3) – (S6) into equation (S2) and simplifying leads to

$$x_b = \frac{\left[W^2 - 12\left(\frac{\rho_i}{\rho_w}\right)^2 H^2\right] \sin \theta + W^2 \sec \theta \tan \theta}{24 \frac{\rho_i}{\rho_w} H}. \quad (\text{S7})$$

The horizontal distance between the center of gravity and the center of buoyancy can then be found from equations (S7) and (S1):

$$\Delta x \equiv x_b - x_g = \frac{\left[12 \frac{\rho_i}{\rho_w} \left(\frac{\rho_i}{\rho_w} - 1\right) H^2 + W^2\right] \sin \theta + W^2 \sec \theta \tan \theta}{24 \frac{\rho_i}{\rho_w} H}. \quad (\text{S8})$$

We can simplify this somewhat by defining $\alpha \equiv \rho_i/\rho_w$ and $\epsilon \equiv W/H$:

$$\Delta x = \frac{H}{2} \left[\left(\alpha - 1 + \frac{1}{12\alpha} \epsilon^2 \right) \sin \theta + \frac{1}{12\alpha} \epsilon^2 \sec \theta \tan \theta \right], \quad (\text{S9})$$

which corresponds to equation (1) in the main text. Performing a Taylor series in θ around 0 gives

$$\Delta x = \frac{H}{2} \left(\alpha - 1 + \frac{\epsilon^2}{6\alpha} \right) \theta + \mathcal{O}(\theta^2),$$

which corresponds to equation (2) in the main text.

Accounting for increasing density with depth

Weeks and Mellor (1978) attempt to account for the density of an iceberg increasing with depth. This lowers the center of gravity by a distance Δ . Weeks and Mellor (1978) consider an iceberg of thickness $H = 200$ m, and they specify $\Delta = 6$ m.

Upon rotation by θ , the horizontal coordinate of the adjusted center of gravity, x'_g , can be seen to be

$$x'_g = -H \left(\frac{\rho_i}{\rho_w} - \frac{1}{2} + \frac{\Delta}{H} \right) \sin \theta = x_g - \Delta \sin \theta,$$

where x_g is the value defined above (S1) for an iceberg of uniform density. The adjusted horizontal distance between the center of buoyancy and the center of gravity is then

$$\Delta x' = \Delta x + \Delta \sin \theta.$$

Computing a Taylor series for θ as above leads to

$$\Delta x' = \frac{H}{2} \left(\alpha - 1 + \frac{\epsilon^2}{6\alpha} + \frac{2\Delta}{H} \right) \theta + \mathcal{O}(\theta^2).$$

Solving for the critical value $\epsilon = \epsilon_c$, which occurs when $\Delta x' = 0$, gives

$$\epsilon_c = \sqrt{6\alpha(1-\alpha) - 12\alpha\frac{\Delta}{H}},$$

which corresponds to equation (4) in the main text.

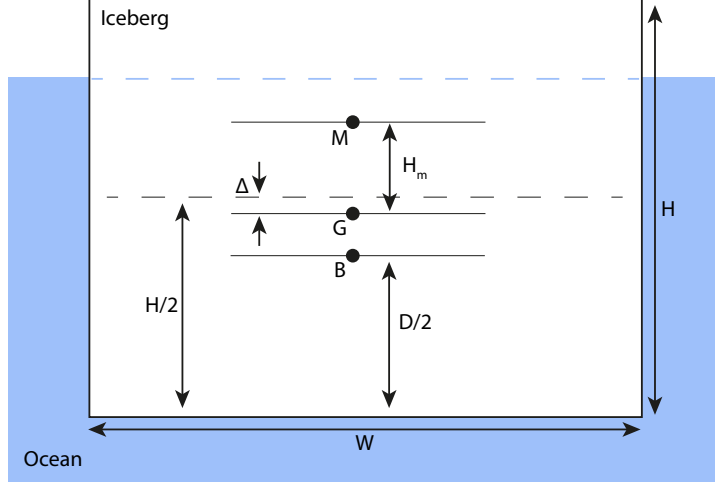


Figure S2. Schematic of a free-floating iceberg indicating the width W , height H , draft D , center of gravity G , center of buoyancy B , metacenter M , metacentric height H_m , and density correction Δ .

Rolling criterion as derived by Weeks & Mellor (1978)

Weeks & Mellor (1978) determine the rotational stability of an iceberg using the metacentric height, H_m (see Fig. S2). The metacentric height is defined as the vertical distance between the center of gravity (G) and the metacenter (M), such that $H_m = M - G$, and it is commonly used to assess the stability of ships. The metacenter is given by $M = I/A + B$, where B is the center of buoyancy, A is the submerged cross-sectional area, and $I = W^3/12$ is the second moment of the area. The submerged area can be written as $A = \alpha HW$ and the center of buoyancy as $B = \alpha H/2$. For an iceberg of uniform density, the center of gravity is simply at $G = H/2$. However, WM78 account for an increase in ice density with depth, as described above. This is done by introducing a correction height, Δ , such that $G = H/2 - \Delta$. The metacentric height can then be written as

$$H_m \equiv \frac{I}{A} - (G - B) = \frac{W^2}{12\alpha H} - \frac{H}{2}\left(1 - \alpha - \frac{2\Delta}{H}\right). \quad (\text{S10})$$

The iceberg will become unstable and roll over when $H_m < 0$. Setting $H_m = 0$ in equation (S10) and solving for the critical width-to-height ratio, $\epsilon \equiv W/H = \epsilon_c$, leads to

$$\epsilon_c = \sqrt{6\alpha(1-\alpha) - 12\alpha\frac{\Delta}{H}}, \quad (\text{S11})$$

which corresponds to equation (4) in the main text. However, Weeks & Mellor (1978) erroneously determined the distance between the center of buoyancy and the center of gravity to be $B - G = H(1 - \alpha)/2 + \Delta$, instead of the correct value $B - G = H(1 - \alpha)/2 - \Delta$ (note that in their notation the iceberg height is given as T). This leads to the erroneous stability criterion

$$\epsilon_c = \sqrt{6\alpha(1 - \alpha) + 12\alpha \frac{\Delta}{H}}$$

which was adopted in a number of subsequent studies, as discussed in the main text.

Iceberg mass evolution for Northern and Southern Hemispheres

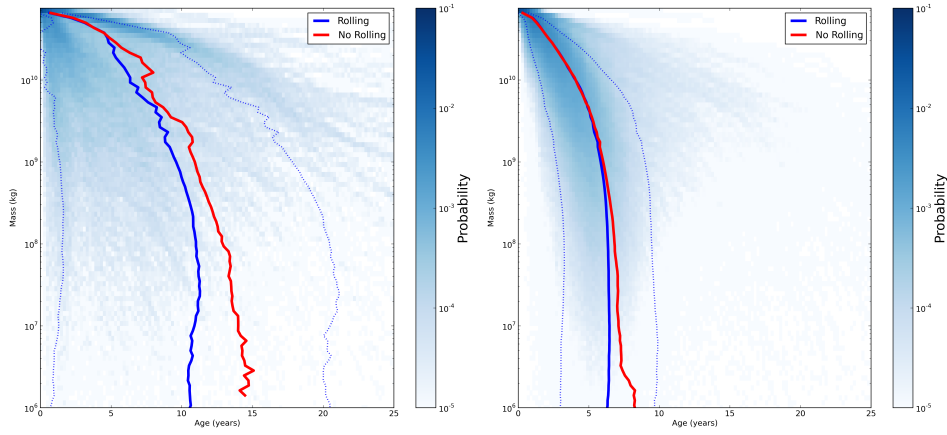


Figure S3. As Fig. 7 in the main text, but for Northern Hemisphere icebergs (left) and Southern Hemisphere icebergs (right).